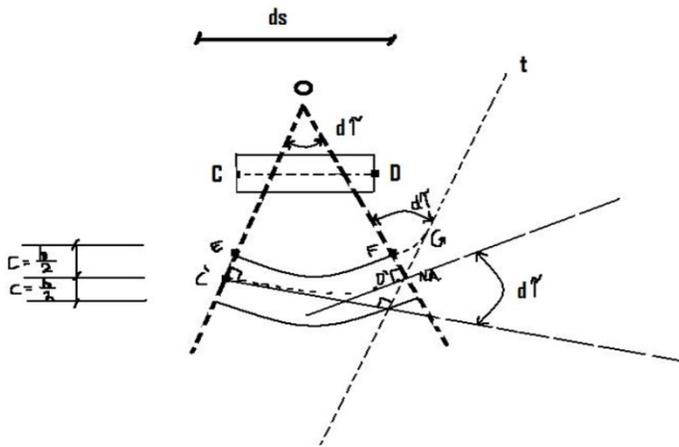
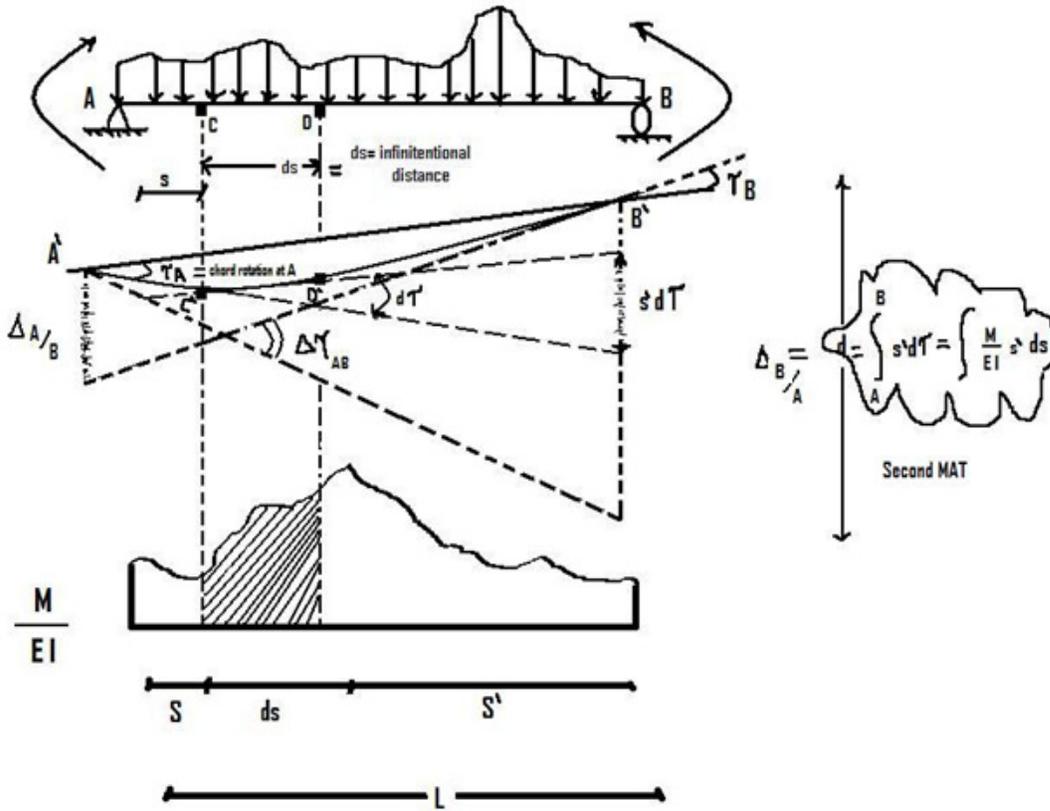


Deflection Computation: Moment Area Theorems (M.A.T.)



Also, $FG = C d \tau$

- From point D' , draw line $D't // OC'$
- Consider deformed beam segment $C'D'$ on the neutral Axis (N.A.). The angle between 2 tangent lines at C' and D' is $d\tau$
- Hence: $\widehat{C'OD'} = \widehat{OD't} = d\tau$
- Also curve line EFG is parallel to curve line $C'D'$
- Hence: $EFG \equiv ds$
- $FG = \text{deformation} = \epsilon ds = \left(\frac{\sigma_c}{E}\right) ds$

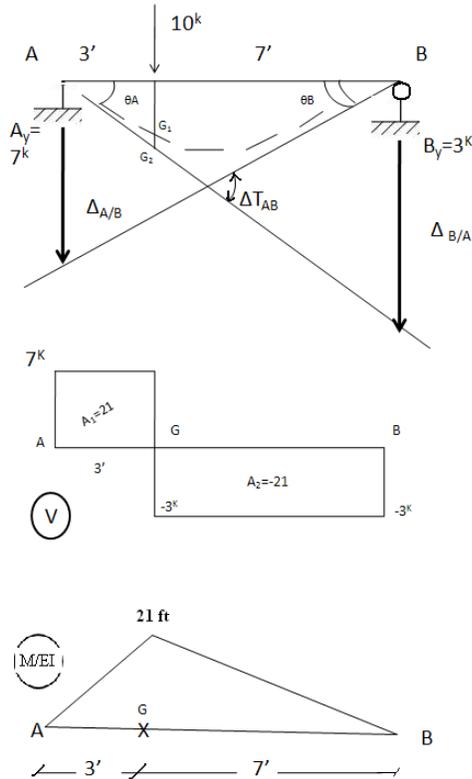
- Hence $\left(\frac{\sigma_c}{E}\right) ds = C d\tau$
 - $\left(\frac{MC}{IE}\right) ds = C d\tau$
- or $d\tau = \frac{M}{EI} ds \Rightarrow \Delta\tau_{AB} = \int \frac{Mds}{EI} \Rightarrow 1^{\text{st}} \text{ M.A.T.}$

Notes:

The first and the second Moment Area Theorems (M.A.T.) will **NOT** directly give the rotation and displacement of a joint on the beam (or frame).

However, M.A.T will compute the **change in angle** (such as $\Delta\tau_{AB}$) between any 2 points (such as A', B') on the beam, and compute the **vertical** distance (such as d or $\Delta_{B/A}$) between 2 tangent lines (at A', B') on the beam.

Example 1: Use Moment Area Theorems (MAT), find the vertical displacement at point G (= δ_G ?) and the rotations θ_a and θ_b at points A and B.



$$\delta_G \equiv GG_1 = (GG_2) - G_1G_2 = (3/10 * \Delta_{B/A}) - \Delta_{G/A}$$

Where:

$$\Delta_{B/A} \stackrel{2nd\ MAT}{=} (\text{Area under } \frac{M}{EI} \text{ diagram})_{\text{between B and A}} *$$

(S' = distance from B to centroid of area)

$$\text{Or: } \Delta_{B/A} = \left(\frac{1}{2} * 21^{Kft} * 7'\right) * \left(S'_2 = \frac{2}{3} * 7'\right) + \left(\frac{1}{2} * 21^{Kft} * 3'\right) * \left(S'_1 = 7' + \frac{1}{3} * 3'\right)$$

$$\Delta_{B/A} = \frac{595}{EI}$$

$$\text{And } \Delta_{G/A} = (\text{area under } M/EI \text{ diagram})_{\text{between B and A}} *$$

(S' = distance from to centroid of area)

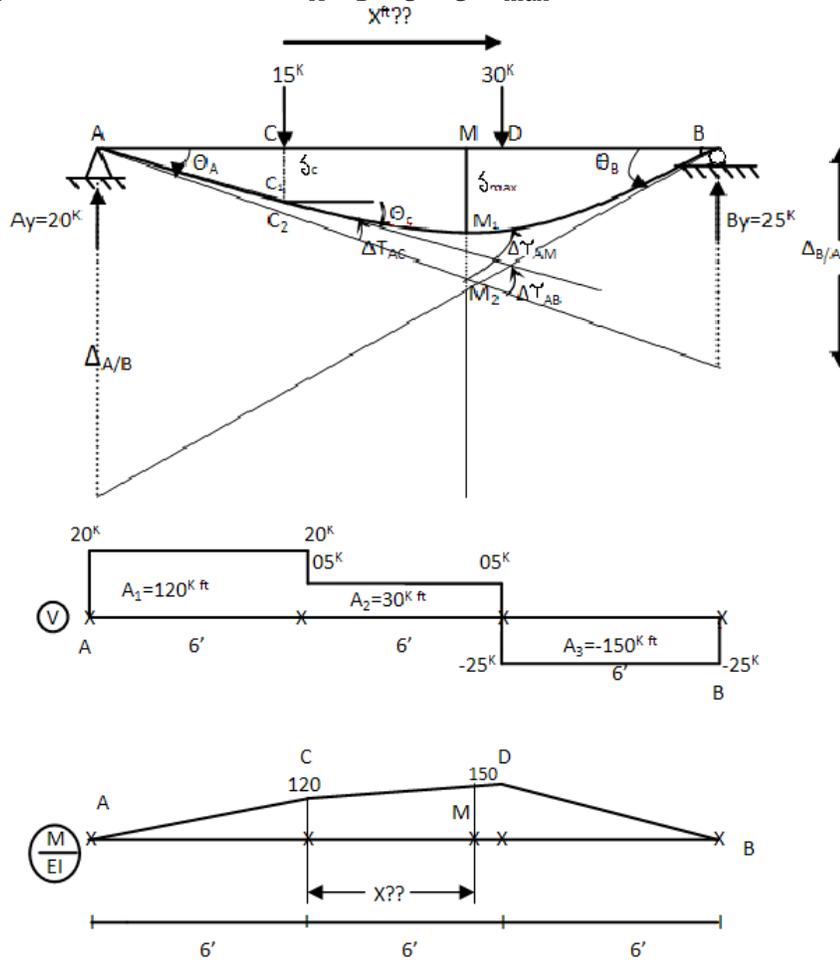
$$\text{Or } \Delta_{G/A} = \left(\frac{1}{2} * 21^{Kft} * 3'\right) * \left(S' = \frac{1}{3} * 3'\right) = \frac{31.5}{EI}$$

$$\text{Thus: } \delta_G \equiv GG_1 = \left(\frac{3}{10} * \frac{595}{EI}\right) - \frac{31.5}{EI} = \frac{147}{EI} = \delta_G$$

$$\theta_A = \text{small angle} = \frac{\Delta_{B/A}}{10'} = \frac{59.5}{EI} = \theta_A$$

$$\theta_B = \text{small angle} = \frac{\Delta_{A/B}}{10} = \left(\frac{1}{10}\right) \left\{ \left(\frac{1}{2} * 3' * 21^{Kft}\right) * \left(\frac{2}{3} * 3'\right) + \left(\frac{1}{2} * 7' * 21^{Kft}\right) \left(3' + \frac{1}{3} * 7'\right) \right\}$$

Example 2: Use M.A.T to find $\theta_A, \theta_B, \theta_C, \delta_C, \delta_{max}$



$$\theta_A \cong \frac{\Delta_{B/A}}{18 \text{ ft}} \dots\dots\dots (1)$$

Where:

$$\Delta_{B/A} = (\text{Area}) * (S' = \text{distance from B to centroid area})$$

$$\Delta_{B/A} = \begin{cases} \left(\frac{1}{2} * 6' * 120 \right) * (S_1' = 12 \text{ ft} + \frac{1}{3} * 6 \text{ ft}) \\ + \left(\frac{1}{2} * 6' * 30 \right) * (S_2' = 6 \text{ ft} + \frac{1}{3} * 6 \text{ ft}) \\ + \left(6' * 120 \right) * (S_3' = 6 \text{ ft} + \frac{1}{2} * 6 \text{ ft}) \\ + \left(\frac{1}{2} * 6' * 150 \right) * (S_4' = \frac{2}{3} * 6 \text{ ft}) \end{cases}$$

$$\text{or } \Delta_{B/A} = \frac{+14,040}{EI} \dots\dots\dots (1^B)$$

$$\text{So: } \theta_A = \frac{\Delta_{B/A}}{18 \text{ ft}} = \boxed{\frac{780}{EI} = \theta_A}$$

Similarly, $\theta_B \cong \frac{\Delta_{A/B}}{18\text{ft}} \dots\dots\dots(2)$

Where: $\Delta_{A/B} = (\text{Area under } \frac{M}{EI} \text{ diagram})_{\text{Between A \& B}} * (S' = \text{distance from A to centroid area})$

$$\Delta_{A/B} = \left\{ \begin{aligned} & \left(\frac{1}{2} * 6' * 120 \right) (S_1' = \frac{2}{3} * 6') + \left(\frac{1}{2} * 6' * 30 \right) (S_2' = 6\text{ft} + \frac{2}{3} * 6\text{ft}) \\ & + \left(6' * 120 \right) (S_3' = 6' + \frac{1}{2} * 6') + \left(\frac{1}{2} * 6' * 150 \right) (S_4' = 12\text{ft} + \frac{1}{3} * 6') \end{aligned} \right.$$

$$\Delta_{A/B} = (360) (4) + (90) (10) + (720) (9) + (450) (14) = \frac{+15,120}{EI}$$

Hence: $\theta_B = \frac{\Delta_{A/B}}{18} = \frac{840}{EI}$

Remarks:

1. The area between A&B (of the $\frac{M}{EI}$ diagram) has been decomposed into three (3) triangulars and one (1) rectangular
2. We can also calculate θ_B , as following:

$$\theta_B = \overset{\oplus}{=} \theta_A + \Delta\tau_{AB} \quad (= \text{angle, rotation at A} + \text{change in angle between A\&B})$$

$$\text{Where: } \Delta\tau_{AB} \equiv (\text{Area of } \frac{M}{EI} \text{ diagram})_{\text{Between A\&B}} = \left\{ \begin{aligned} & \left(\frac{1}{2} * 6' * 120 \right) + \left(\frac{1}{2} * 6' * 30 \right) \\ & + \left(6' * 120 \right) + \left(\frac{1}{2} * 6' * 150 \right) \end{aligned} \right.$$

Or $\Delta\tau_{AB} = \frac{1620}{EI}$

Hence: $\theta_B = (\theta_A = \overset{\curvearrowright}{\text{cw}} - \frac{780}{EI}) + \left(+ \frac{1620}{EI} = \Delta\tau_{AB} \right) = \frac{+840}{EI} = \theta_B$

↖
↖

ccw
ccw

- Also : $\theta_C = \theta_A + \Delta\tau_{AC}$ (3)

Where $\theta_A = \frac{cw\ 780}{EI}$

And $\Delta\tau_{AB} = 1^{st}\ M.A.T = (\text{area under } \frac{M}{EI} \text{ diagram})_{\text{between A\&C}}$

$$\Delta\tau_{AC} = \left(\frac{1}{2} * 6' * 120\right) = + \frac{360}{EI}$$

Because CCW (see picture previous page)

Hence $\theta_C = \left(\frac{-780}{EI}\right) + \left(\frac{+360}{EI}\right) = \boxed{\frac{cw\ 420}{EI} = \theta_C}$

- From the figure, one has:

$$\delta_C \equiv CC_1 = (CC_2) - [C_1C_2] \quad (4)$$

Or $\delta_C = \left(\frac{6\ ft}{18ft} * \Delta_{B/A}\right) - [\Delta_{C/A}] \quad (5)$

Where: $\Delta_{C/A} = 2^{nd}\ M.A.T. = (\text{area under } \frac{M}{EI})_{\text{Between C \& A}} *$

(S' = distance from C to centroid area)

$$\text{Or } \Delta_{C/A} = \left(\frac{1}{2} * 6' * 120\right) * (S' = \frac{1}{3} * 6') = \frac{720}{EI}$$

Hence: $\delta_C = \left(\frac{6}{18} * \frac{14,040}{EI}\right) - \left[\frac{720}{EI}\right] = \boxed{\frac{3960}{EI} = \delta_C}$

- To find δ_{\max} (located at point M on the beam)

Notes $\begin{cases} \rightarrow \text{Point M (with max. deflection) should be close to } 30^k \text{ load} \\ \rightarrow \text{Rotation at point M } (\theta_M) \text{ should be zero} \end{cases}$

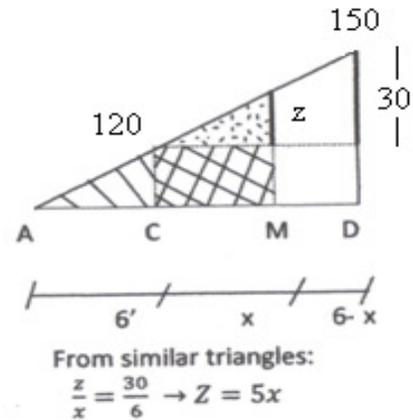
We have: $\theta_M \stackrel{\oplus}{=} \theta_A + \Delta\tau_{AM}$ _____ (6)

$$0 = \left(-\frac{720}{EI}\right) + \Delta\tau_{AM}$$
 _____ (7)

Where:

$$\Delta\tau_{AM} = \left(\text{Area under } \frac{M}{EI} \text{ Between A\&M}\right)$$

$$\Delta\tau_{AM} = \begin{cases} \left(\frac{1}{2} * 6' * 120\right) \\ + (1/2 * x * [z = 5x]) \\ + (120 * x) \end{cases}$$

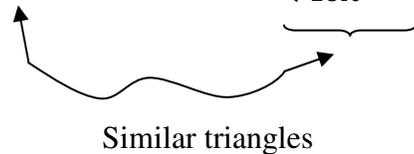


$$\Delta\tau_{AM} = (360) + (2.5x^2) + (120x)$$
 _____ (8)

Substitute Eq (8) into Eq (7) to obtain:

$$0 = \left(-\frac{780}{EI}\right) + \left(\frac{+2.5x^2 + 120x + 360}{EI}\right) \rightarrow x = 3.28 \text{ ft}$$

Thus: $\delta_{\max} \equiv (MM_2) - M_1M_2 = \left(\frac{9.26\text{ft}}{18\text{ft}} * \Delta_{B/A}\right) - [\Delta_{M/A}]$ _____ (9)



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Where: $\Delta_{M/A}$ (Use 2nd M.A.T.) = (area under $\frac{M}{EI}$)_{Between M & A} * (S' = distance from M to centroid area)

$$\Delta_{M/A} = \left\{ \begin{array}{l} \left(\frac{1}{2} * 6' * 120 \right) * (S_1' = 3.28' + \frac{1}{3} * 6') \\ + \left(\frac{1}{2} * 3.28 * [z = 5 * 3.28'] \right) * (S_2' = \frac{1}{3} * 3.28') \\ + (120 * 3.28) * (S_3' = \frac{1}{2} * 3.28') \end{array} \right.$$

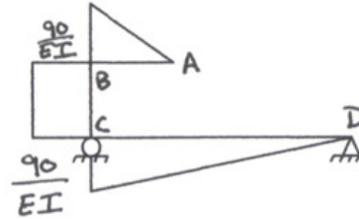
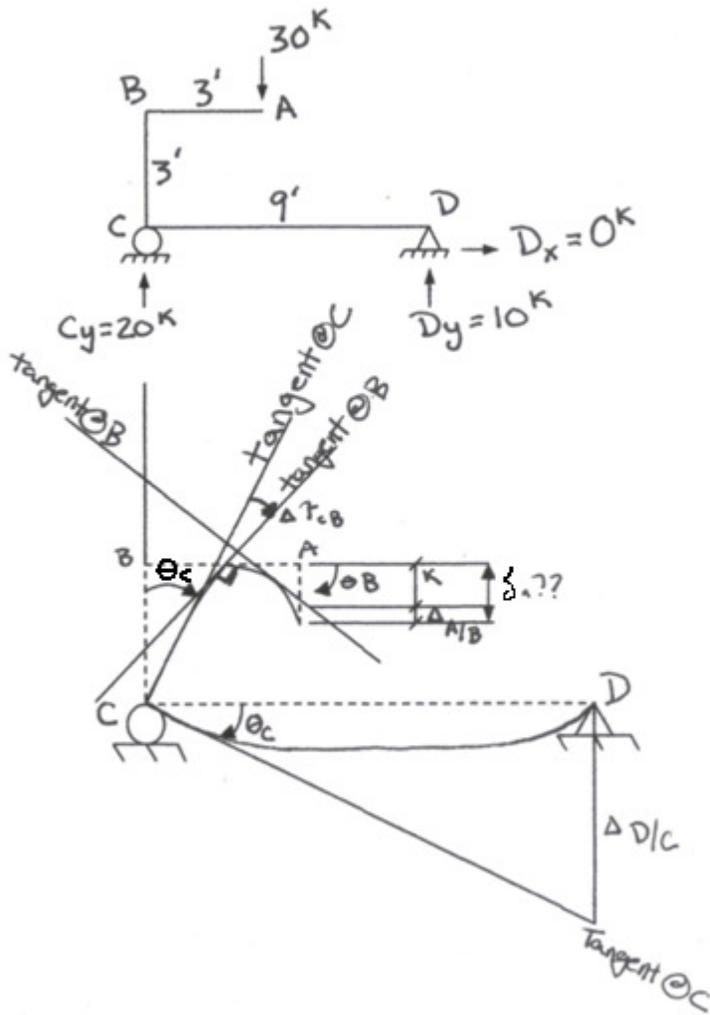
$$\Delta_{M/A} = (360) * (5.28') + (1.64) * (16.4) * (1.09) + (393.6) * (1.64) = \frac{2575.6}{EI} = \frac{2575.6}{EI} \quad (10)$$

Substituting Eq. (10) of Eq. (1^B) into Eq. (9), to get:

$$\delta_{\max} = \frac{9.28^{\text{ft}}}{18\text{ft}} * \frac{14,040}{EI} - \left[\frac{2575.6}{EI} \right]$$

$$\boxed{\delta_{\max} = \frac{4662.8}{EI}}$$

Example 3 Use Moment Area Theorems (M.A.T.), find the vertical deflection at joint A (δ_A) of the frame structure.



(M/EI) Diagram

Moments Plotted on Tension Side

Strategies:

- **Step 1:** Compute $\Delta_{D/C}$ (use 2nd M.A.T)
- **Step 2:** $\theta_C \cong \frac{\Delta_{D/C}}{9 \text{ ft}}$
- **Step 3:** Compute $\Delta\tau_{CB}$ = Change in angle between tangent lines @ C & B (used 1st MAT)
- **Step 4:** $\theta_B = \theta_C + \Delta\tau_{C/B}$
- **Step 5:** $K \cong (3^{\text{ft}}) * \theta_B$
- **Step 6:** Compute $\Delta_{A/B}$ (use 2nd MAT)
- **Step 7:** $\delta_A = K + \Delta_{A/B}$

Step 1: $\Delta_{D/C} = (\text{area of } \frac{M}{EI})_{D \rightarrow C} * (S' = \text{distance from D to centroid area})$
 $= (\frac{1}{2} * \frac{90}{EI} * 9\text{ft}) * (S' = \frac{2}{3} * 9\text{ft}) = \frac{2430}{EI}$

Step 2: $\theta_C = \frac{2430}{9EI} = \frac{270}{EI}$

Step 3: $\Delta\tau_{CB} = (\text{area of } \frac{M}{EI})_{C \rightarrow B} = \frac{90}{EI} * 3\text{ft} = \frac{270}{EI}$

Step 4: $\theta_B \overset{\oplus}{=} (\frac{270}{EI}) + (\frac{+270}{EI}) = (\frac{540}{EI})$

Step 5: $K = 3 * (\frac{540}{EI}) = \frac{1620}{EI}$

Step 6: $\Delta_{A/B} = (\text{area of } \frac{M}{EI})_{A \rightarrow B} * (S' = \text{distance from A to centroid area})$
 $= (\frac{1}{2} * \frac{90}{EI} * 3\text{ft}) * (S' = \frac{2}{3} * 3\text{ft}) = \frac{270}{EI}$

Step 7: $\delta_A = \frac{1620}{EI} + \frac{270}{EI} = \boxed{\frac{1890}{EI} = \delta_A}$